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# EXAMPLES AND PRINCIPLES OF MATHEMATICAL MODELLING IN MEDICINE: ULTRASOUND

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# 1. Physical Principles

## Piezo-electricity

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Ultrasound works because of two related properties: when an electric current is applied the material moves. This is called the **inverse piezo-electric effect** and this is used to generate the sound field.

When the material experiences a mechanical stress, it generates a charge. This is used the **piezo-electric effect** and is used to generate the signal which is reconstructed to form an image.

Ultrasound is sound above 26.5 kHz, above the range of human hearing, but in medical applications the frequencies are in the mega Hertz regime ( $10^6$  cycles per second).

# 1. Physical Principles

## Therapeutic Transducers

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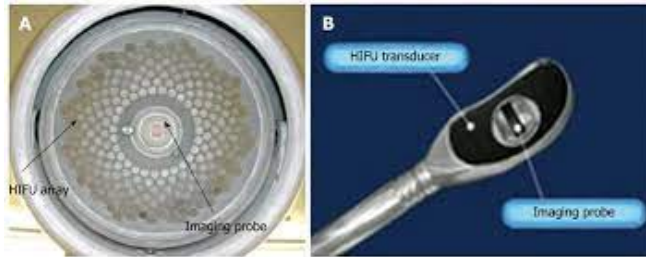


Figure: Image from [17]

# 1. Physical Principles

## Therapeutic Ultrasound

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As the acoustic wave (longitudinal) passes through the body it is absorbed. This leads to a rise in temperature.

When a continuous wave, high intensity focused ultrasound, **HIFU**, can be used as a therapy to heat tissue.

If the waves are very intense, ultrasound can be used to mechanically damage tissue. For the destruction of kidney stones this is call **lithotripsy**; the destruction of soft tissue this is called **histotripsy**.

# 1. Physical Principles

## Therapeutic & Diagnostic Ultrasound

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Ultrasound is a cheap, real-time, portable **imaging** modality which can generate lots of data easily. Because of these reasons there are many machine-learning algorithms which are used to enhance the low-contrast, noisy images. A disadvantage is that it is operator dependent.

As a **therapy**, ultrasound is cost-effective, non-ionising, non-invasive, monitorable and able to selectively destroy small regions of tissue deep with the body.

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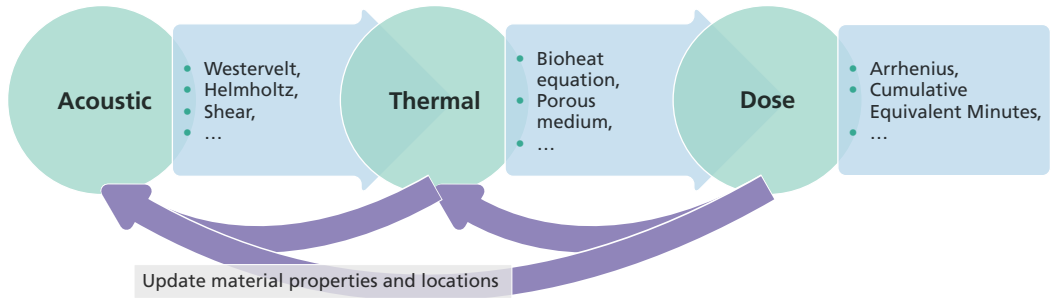
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1. Physical Principles
- 2. Fundamentals of Modelling Ultrasound**
3. Nonlinearity
4. Attenuation
5. Dose
6. Open Problems

## 2. Fundamentals of Modelling Ultrasound

### Typical Simulation Pipeline

In the context of therapeutic ultrasound:



## 2. Fundamentals of Modelling Ultrasound

### Westervelt Equation

From first principles 14 quantities are required to model the acoustic wave propagation. Fortunately this can be reduced down to 7, then 5, then down to a single variable: pressure,  $p$

$$\frac{\partial p}{\partial z} = \underbrace{\frac{c_0}{2} \int_{-\infty}^t \nabla^2 p \, d\tau}_{\text{Diffraction}} + \underbrace{\frac{2}{c_0^3} \mathcal{L}[p; \alpha_0, \eta]}_{\text{Attenuation}} + \underbrace{\frac{\beta}{2\rho c_0^3} \frac{\partial p^2}{\partial t}}_{\text{Nonlinearity}}$$

captures the three key physical phenomena of

- Diffraction: the property of a wave to spread as it propagates
- Attenuation: the absorption of the wave by the medium
- Nonlinearity: the change in the wave form as it propagates



## 2. Fundamentals of Modelling Ultrasound

### Computation Challenges

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HIFU encounters a challenge in the computation of the state equations: for example implicit, stable finite-difference time-domain codes in a clinically relevant imaging context [12] requires calculations of the order of **exaflops**

$$\text{exaflop} \quad 10^{18} = 1,000,000,000,000,000,000$$

extremely computationally expensive

## 2. Fundamentals of Modelling Ultrasound

### Ultrasound

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The formulation of the governing equation and, consequently the solution method, is dependent on the application.

- Is the wave pulsed or running continuously? Harmonic solution can be assumed
- Are there significant scatterers in the domain? One-way solutions could be used.
- Is the input power high? Does nonlinear propagation need to be considered?
- Is the transducer a single element or an array? Is it curved or flat?

The review [6] provides an overview of the methods.

## 2. Fundamentals of Modelling Ultrasound

### Linear: Helmholtz

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In the linear case, continuous wave case the acoustic Helmholtz equation is derived.

This can be solved by in many ways, for example by finite-elements, or by boundary elements methods.

$$G_{i,j} = \int_{\partial\Omega} G(x, x_i) \varphi(y_j) ds \quad \text{and} \quad H_{i,j} = \int_{\partial\Omega} G_n(x, x_i) \varphi(y_j) ds$$

The assembly of the boundary element matrix is costly, but can be accelerated by either fast multi-pole methods [3] or hierarchical matrix [7] formulations.

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### 3. Nonlinearity

#### Nonlinearity

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Nonlinearity arises from the property that very high/low parts of the waveform travel faster than less intense parts.

The wave steepens.

Consider, in one-dimension, an initially sinusoidal wave  $p = p_0 \sin(\omega t)$ , then

$$\begin{aligned}\frac{\partial p^2}{\partial t} &= p_0^2 \frac{\partial \sin^2(\omega t)}{\partial t} \\ &= 2p_0^2 \omega \sin(\omega t) \cos(\omega t) \\ &= p_0^2 \omega \sin(2\omega t)\end{aligned}$$

Thus nonlinearity results in the generation of **higher frequency components** to the wave equation which are integer multiples of the fundamental frequency.

Note: the equations are **weakly nonlinear** as the particle velocity is less than the speed of sound.

### 3. Nonlinearity

#### Burgers Equation

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In general it is not possible to write down the solution to nonlinear PDEs, but a one-dimensional version of the Westervelt equation is the acoustic Burger's equation

$$\frac{\partial v}{\partial x} - \beta v \frac{\partial v}{\partial t} - \frac{\partial^2 v}{\partial t^2} = 0.$$

where  $v$  is the acoustic velocity.

This is solvable and expressions for nonlinear wave propagation can be derived.

### 3. Nonlinearity

## Wave Steepening

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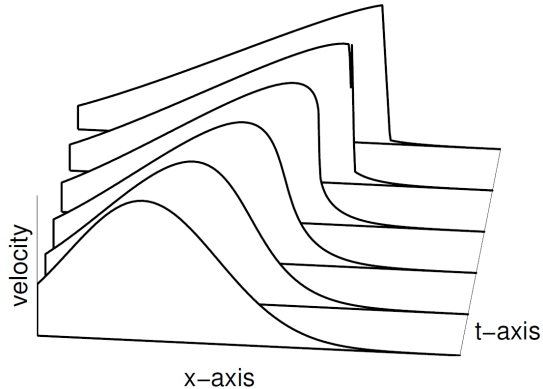


Figure: Evolution of Burgers equation as wave becomes shocked

### 3. Nonlinearity

#### Acoustic to Thermal Coupling

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The source term in the thermal model is given by the **square** of the pressure

$$q_n = 2\alpha I, \quad \text{where} \quad I = \sum_{i=1}^N \frac{p_i^2}{\rho_0 c_0}$$

which is generalised for nonlinear propagation.

There is another **local** absorption mechanism which may be included in applications in which **shock-like** waves may be present

$$q_s = \frac{\beta f_0 A_s^3}{6c_0^4 \rho_0^2}$$

The heating is **independent** of attenuation coefficient. It scales against the **cube** of the shock height,  $A_s$ .



### 3. Nonlinearity

#### Shock-like Waves

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Tissue is attenuating thus “true” shocks will never occur. So how do we specify when this form of heating will occur? That is, what is the difference between a nonlinear wave and a shock-like wave?

The means to distinguish between the two is to observe that shock-like waves will have a finite **shock width**.

The physical shock width for acoustic Burgers' equation is of the order  $\mathcal{O}(\varepsilon)$ , where  $\varepsilon$ , called the Goldberg number, is the ratio of nonlinearity to attenuation [5].

### 3. Nonlinearity

#### Shock Enhances Heating

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However, when using an operator-splitting approach the resolution of the shock width [10] is typically  $\mathcal{O}(\sqrt{k\varepsilon})$ . So the spatial resolution,  $h$ , must be adjusted accordingly, i.e.  $h \sim \varepsilon$ , to match the physical shock width.

Thus, by using exact analytical expression for appearance of shock-like wave, it is possible to compute the contribution from shock enhanced heating.

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## 4. Attenuation

### Attenuation

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Attenuation is comprised of absorption and scatter. There are two fundamental processes which determine absorption:

- **Viscous heating:** absorption is proportional to the square of the frequency:  $\mathcal{L} \sim \omega^2 \rightarrow \frac{\partial^2 p}{\partial t^2}$ . At frequencies for medical ultrasound this mechanism is relevant for water.
- **Relaxation processes:**  $\mathcal{L} \rightarrow \frac{\partial \xi}{\partial t}$ , where  $\dot{\xi} = \alpha \xi + \beta + \nabla p$ . In media with a complex molecular structure, such as tissue, there are a huge number of relaxation processes and the absorption is accurately modelled by a powerlaw:  $\mathcal{L}[\omega] \sim \omega^\eta$ , where  $\eta = 1 + \nu$ .

## 4. Attenuation

### Single Relaxation Process

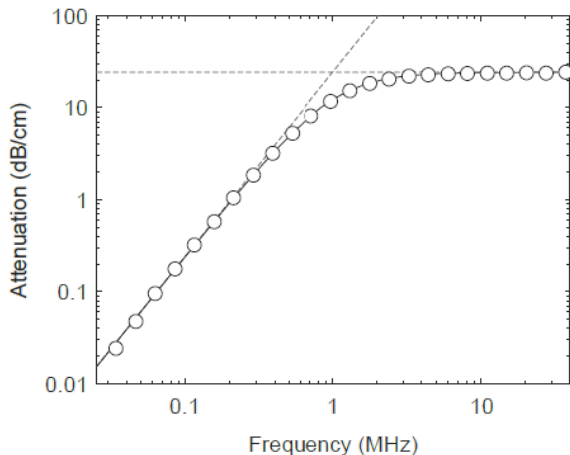


Figure: From [11]

## 4. Attenuation

### Tissue Data

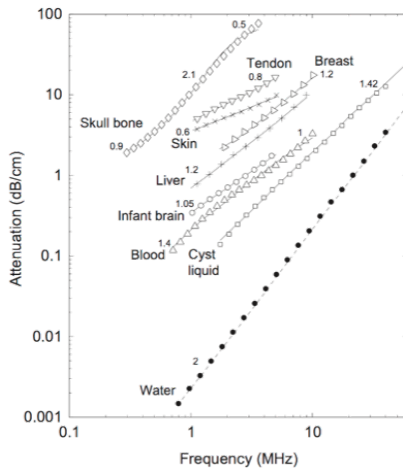


Figure: From [9]

## 4. Attenuation

### Powerlaw Absorption

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For linear propagation each frequency can be solved independently for a given attenuation factor derived from experiments.

But in general, the frequency-dependent powerlaw for attenuation can lead to an convolutional integral [15]

$$\mathcal{L}[p] = \int_0^t J(\tau - t_0) \star p(\tau) d\tau$$

or as via a **fractional operator** in time

$$= \frac{\partial^\nu p}{\partial t^\nu}$$

How this is handled is dependent on the clinical context - whether ultrasound is pulsed or continuous wave.

## 4. Attenuation

### Gamma Function

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The gamma function is defined as:

$$\Gamma(s) = \int_0^{\infty} t^{s-1} e^{-t} dt$$

As

- $\Gamma(1) = 1$

and

- $\Gamma(n) = n\Gamma(n-1)$

then

- $\Gamma(n) = (n-1)! \quad \forall n \in \mathbb{N}^+$

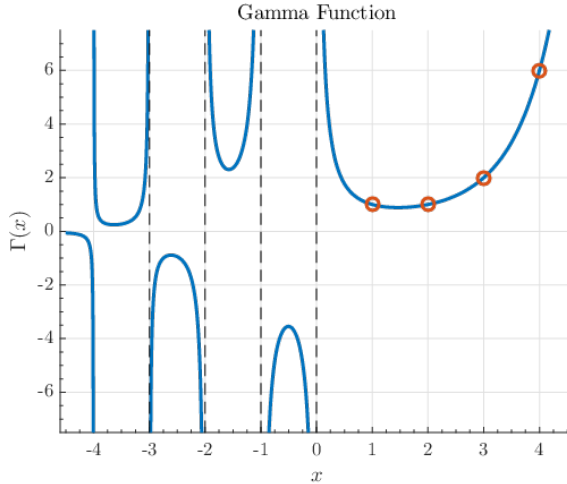
thus the gamma function can generalise the factorial operator.



## 4. Attenuation

### Gamma Function

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## 4. Attenuation

### Fractional Derivatives for Polynomials

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For a simple **monomial** function  $u(x) = x^k$ , with  $k, a \in \mathbb{N}^+$

$$\frac{d^a u}{dx^a} = \begin{cases} \frac{k!}{(k-a)!} x^{k-a} & \text{if } k \geq a \\ 0 & \text{if } k < a \end{cases}$$

Now generalise for  $a \in \mathbb{R}^+$

$$= \frac{\Gamma(k+1)}{\Gamma(k+1-a)} x^{k-a}$$

## 4. Attenuation

### Riemann-Liouville & Caputo Formulations

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The definition of a fractional derivative is more involved for general functions. There are a number of formulations:

- Grünwald-Letnikov
- Riemann-Liouville
- Caputo

Only the Riemann-Liouville formulation ensures that the absorption operator is causal, however, it is more complicated to implement numerically and, requires initial conditions which are difficult to ascertain experimentally.

## 4. Attenuation

### Repeated Integrals

The fractional derivative relies on the definition of the fractional integral. Let an integration operator be:

$$\mathcal{I}_\alpha [u](x) = \int_\alpha^x u(t) dt$$

applied again

$$\mathcal{I}_\alpha^2 [u](x) = \int_\alpha^x \left( \int_\alpha^t u(s) ds \right) dt.$$

Cauchy showed

$$\mathcal{I}_\alpha^n [u](x) = \frac{1}{(n-1)!} \int_\alpha^x (x-t)^{n-1} u(t) dt.$$

This is easily generalised to fractional terms.

## 4. Attenuation

### Fractional Derivatives

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The fractional derivative relies on the definition of the fractional integral. But the notion of the fractional integral being the anti-fractional derivative **no longer** holds.

The fractional derivative,  $\mathcal{D}_\alpha^s$  of order  $s \in (k-1, k]$ , with  $k \in \mathbb{N}$  is defined by the  $k^{\text{th}}$ -derivative of the  $(k-s)^{\text{th}}$ -fractional integral

$$\mathcal{D}_\alpha^s [p](x) = \frac{1}{\Gamma(k-s)} \frac{\partial^k}{\partial \tau^k} \left( \int_\alpha^\tau \frac{p(x, s)}{(\tau-s)^{s+1-k}} ds \right)$$

The classical derivative depends locally on the point of evaluation, but fractional derivatives are dependent on **all** values between  $\alpha$  and  $x$ . It is a **non-local** operator. In ultrasound computation requires knowledge over the duration of the exposure.

## 4. Attenuation

### Pseudo-Spectral: $k$ -space

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A common approach is to model the system in  $k$ -space. This means taking the **spatial Fourier** transform in  $(x, y, z)$  and mapping to  $(k_x, k_y, k_z)$ .

As a wave equation, computations are naturally handled in a frequency domain. Another advantage is that the approximation of the derivative is highly accurate, as

$$\hat{p}(k, t + \Delta t) - 2\hat{p}(k, t) + \hat{p}(k, t - \Delta t) = -4 \sin^2(ck\Delta t/2) \hat{p}(k, t) \quad (1)$$

The frequency dependent power-law for attenuation law is expressed as a **fractional Laplacian** [14, 16, 4]

$$\nabla^{\nu/2} p = \nabla^2 (D^{2-\nu} p)$$

Now, the partial differential equation has been transformed into a system of nonlinear ordinary differential equations which are solved in time.

## 4. Attenuation

### Pseudo-Spectral: Spatial Marching

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Another approach is to consider continuous wave exposures and work in pseudo-spectral domain taking the Fourier transform in time and two spatial dimensions  $(x, y)$ , so that a differential equation,  $\hat{p}(k_x, k_y, z, \omega)$  which is solved in space, stepping forward in  $z_i = z_0 + i\delta z$

In this case, the powerlaw, formulated as a fractional operator in time, is simple to handle

$$\frac{\partial^\nu p}{\partial t^\nu} = \mathcal{F}^{-1}((-i\omega)^\nu \mathcal{F}(p)).$$

This formulation assumes an input plane as an initial condition, which typically is given by measurement data.

## 4. Attenuation

### Simulations from Measurements

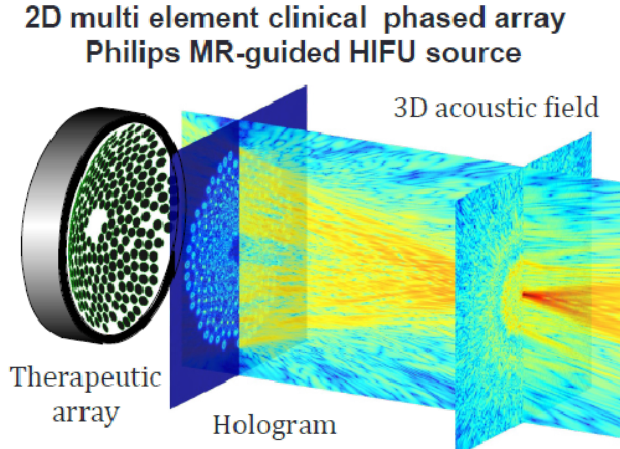


Figure: Image from [13]



## 4. Attenuation

### Quadrature

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Another approach is to handle the quadrature directly.

Or use oblivious quadrature [2]: this approximates the fractional operator

$$\frac{\partial^\nu p}{\partial t^\nu} = \sum_{j=0}^n \omega_{n-j} (p(t_j) - \chi p(0))$$

where the weights  $\omega$  are determined by solving a

$$\left( \frac{3 - 4\xi + \xi^2}{2h} \right)^\nu = \sum_{j=0}^{\infty} \omega_j \xi^j$$

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## 5. Dose

### Dose Equations

Two formulations for the damage,  $\Omega$ ,

- Arrhenius component models, based on chemical kinetic models. For example, the first-order rate equation

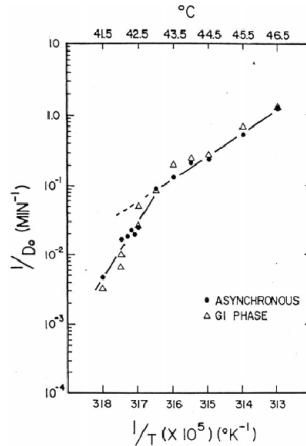
$$[E] \xrightarrow{k_d} [D] \quad \text{leads to} \quad \Omega = \int_0^t A e^{-E_a/(R\bar{T})} ds.$$

- Cumulative equivalent minutes, typically threshold value of an isothermal dose value of 240 min at 43°

$$\Omega = \int_0^t R^{\bar{T}(x,t) - \bar{T}_{\text{ref}}} ds \quad \text{with} \quad \bar{T}_{\text{ref}} = 43^\circ \quad \text{and} \quad R = \begin{cases} 0.25 & \text{for } T < 43^\circ \\ 0.5 & \text{for } T \geq 43^\circ \end{cases}$$

## 5. Dose

### Piecewise Continuous Damage



**Figure:** Many models are based on data from [8] which shows two distinct regimes in which the rates of damage differ.

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## 6. Open Problems

### Open Questions

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- How does power-law absorption system behave for low power, i.e. discarding nonlinearity, does a Green's function exist for the fractional absorption wave equation?
- In the one-dimensional nonlinear case – **fractional Burgers equation** – is the system integrable? Does a Cole-Hopf transformation exist? When do shocks form? What is the shock width?
- Can a better formulation of the thermal dose equations be derived from a more complicated rate-reaction scheme?

## 7. Code

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A key reference is [1], which benchmarks ultrasound code for transcranial applications.

- </> **Comsol**: commercial multiphysics finite element solver – axisymmetric, frequency domain models, with temperature dependency are often used. curvature of transducer accurately resolved
- </> **Sim4Life**: combines human phantoms, tissue properties and solvers. Can solve nonlinear acoustic equations in time-domain.
- </> **k-wave**: open-source matlab ultrasound wave pseudo-spectral simulator for diagnostic and therapeutic applications: compiled C++ and cuda binary can accelerate code.
- </> **FeNiCs**: open source automatic finite element library
- </> **HITU\_Simulator**: A nonlinear axisymmetric beamer simulator (Matlab, GPL-3, GitHub)
- </> **j-wave**: open source implementation of k-wave in JAX (optimised automatic differentiation framework)
- </> **BabelBrain**: open source acoustic solver for transcranial applications
- </> **Bempp**: open source boundary element solver for wave problems

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# Thankyou for your attention

## Any questions?



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github.com/djps



djps.github.io



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